

# RECLAMATION

*Managing Water in the West*

## Incorporating Breach Parameter Estimation and Physically-Based Dam Breach Modeling into Probabilistic Dam Failure Analysis

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U.S. Department of the Interior  
Bureau of Reclamation

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# Issues

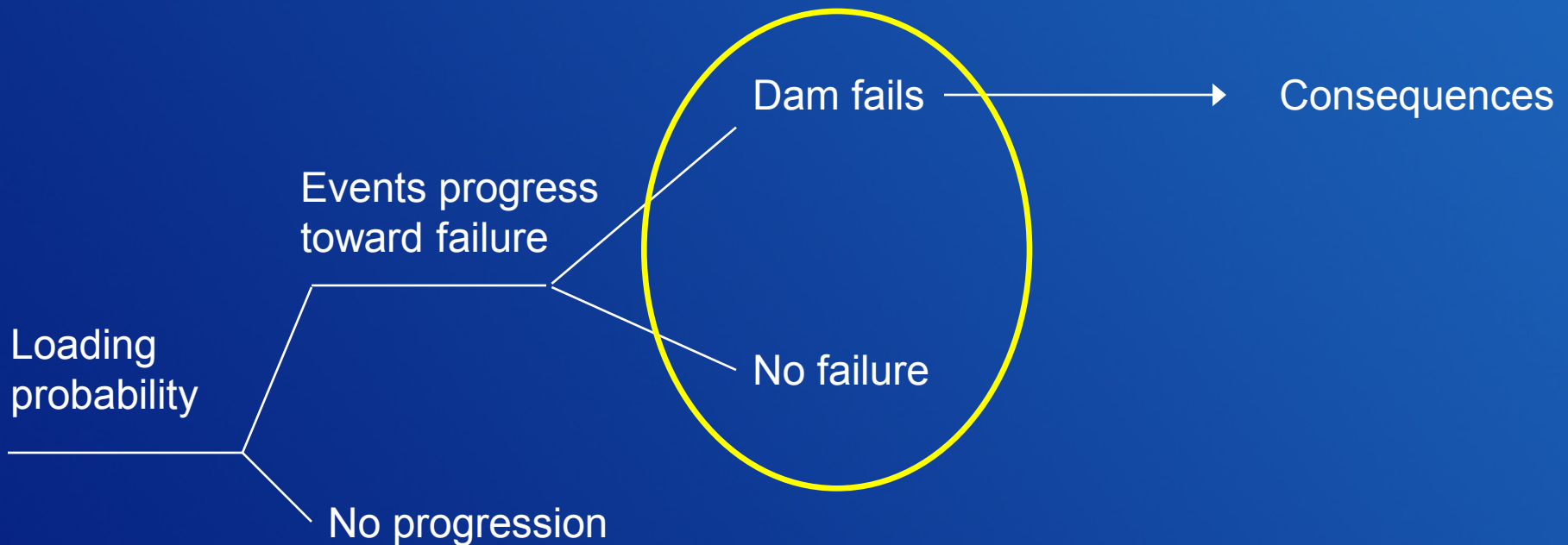
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- **How to evaluate failure probability?**
- **How to estimate breach parameters in a probabilistic way?**
  - Size of breach
  - Shape of breach
  - Time of failure (rate of erosion)
- **Scope of this talk limited to embankment dams**

# Failure Probability

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- Failure probability is a central question



# Hydrologic Failure Modes

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- Is depth and duration of overtopping sufficient to produce unstoppable erosion?
- Can flood surcharge in the reservoir trigger a seepage-erosion sequence that progresses too quickly to stop?



# Riley 1986

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- **First work discussing analysis of limited overtopping that might not cause dam failure**
- **Applied only to cohesive, erosion-resistant embankments protected by well maintained vegetation**
- **Suggested permissible duration-velocity limits for flow over crest and down the slope**
- **Also suggested permissible total volumes of flow in a given duration**

# Riley 1986

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- **Addressed the “will it fail?” question**
  - Suggested conservative thresholds for when failure would occur
- **Did not address the probability of failure question**
  - When thresholds were exceeded, probability of failure was 1

# Fragility Curves

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- **Attempt to estimate probability of failure based on engineering judgment of team members**
  - Depth of overtopping
  - Velocity of flow
  - Duration of overtopping / Volume of water
  - Quality of slope protection (vegetation or riprap)
  - Erodibility of embankment materials
- **Very subjective...**

# New Tools

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- **Physically-based dam breach models**
  - WinDAM (USDA-ARS)
  - HR BREACH (HR Wallingford)
  - Others...

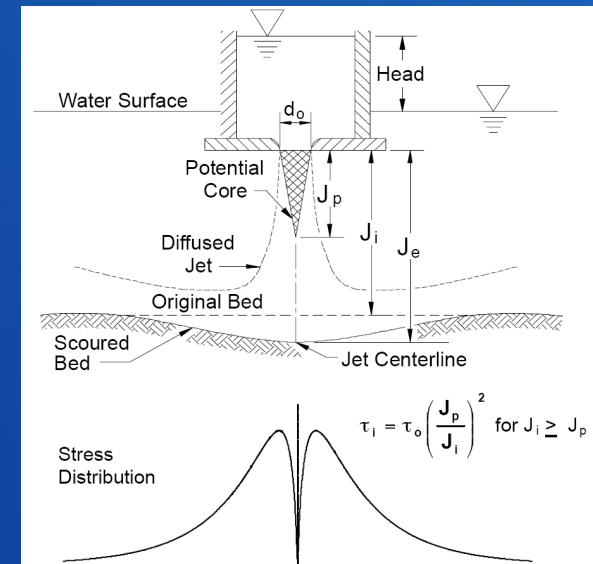
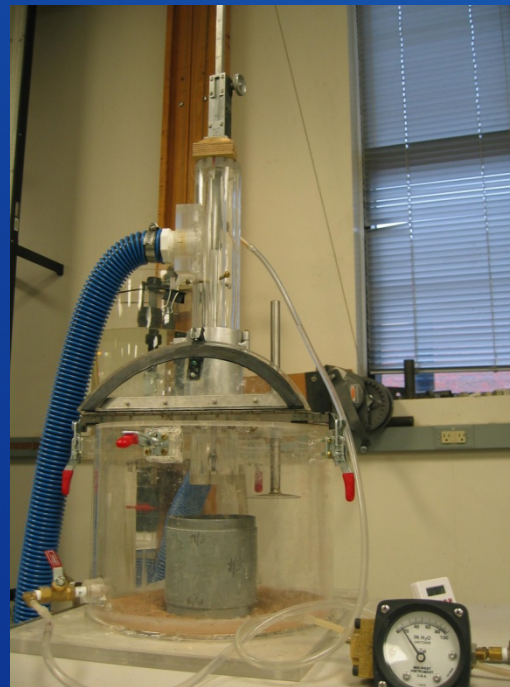


# Dam Breach Models

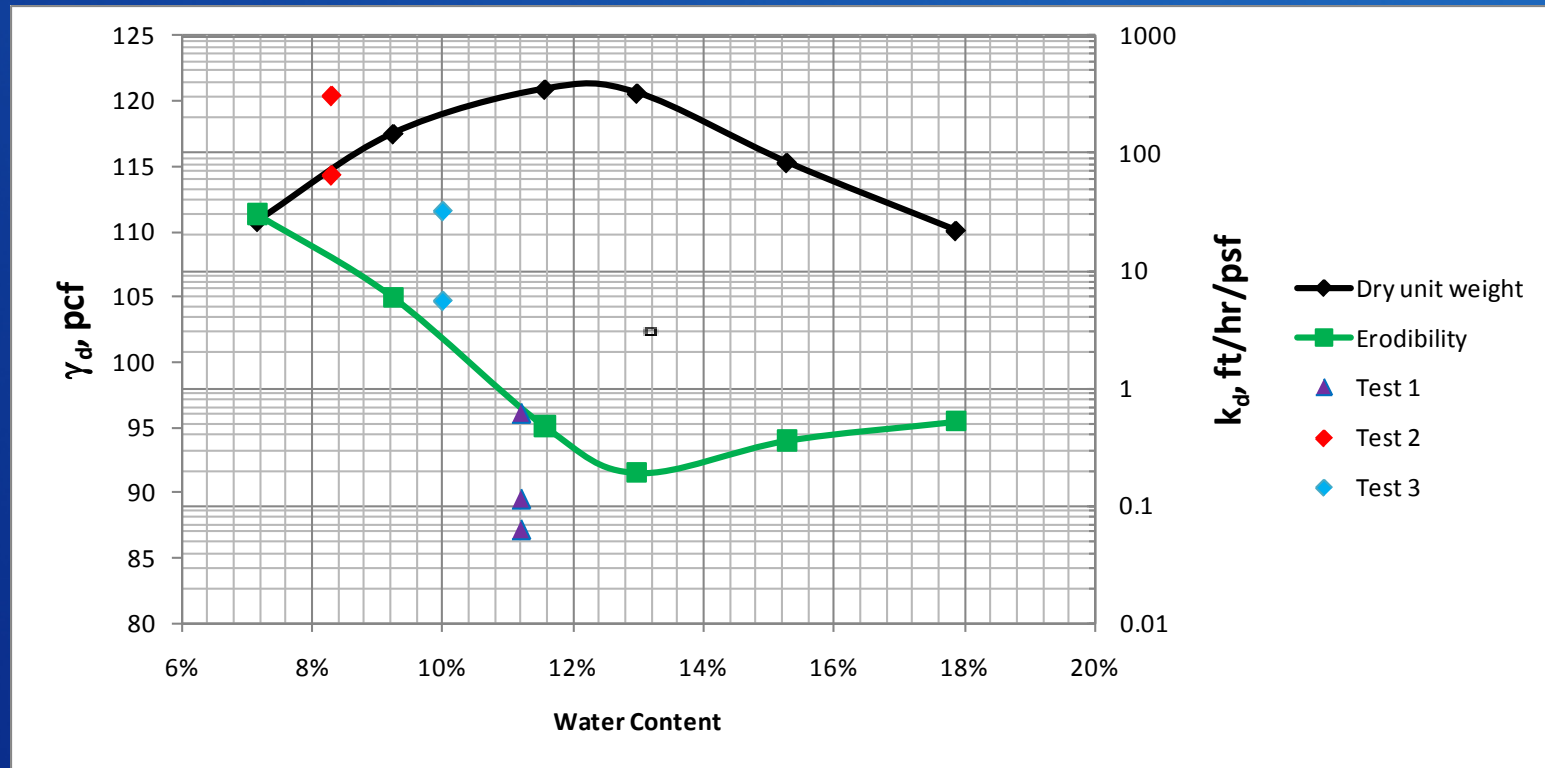
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- **Inputs**
  - Hydraulic attack (overtopping depth, velocity, shear stress, stream power)
  - Slope protection, threshold of failure
  - Erodibility of embankment material (**measured!**)
    - Estimate erosion rates
    - Simulate mechanics of headcut development
  - Simulate extent of erosion during duration of event

# Submerged Jet Test - Erodibility



# Compaction & Erodibility



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# Dam Breach Models

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- **Output**

- Determine whether threshold for failure is reached
- Outflow hydrograph
- Time-history of breach development

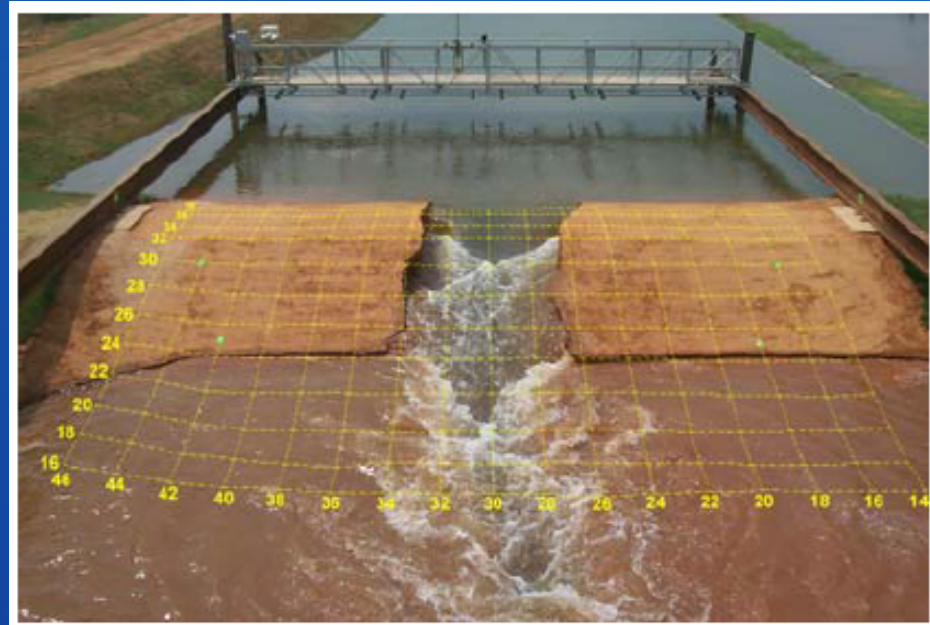
Consequence analysis

- **Probabilistic uses**

- Models run quickly
- Can readily analyze variations in flood loading, slope protection and soil erodibility



# Greg Hanson and Sherry Hunt – USDA-ARS



Soils used in breach widening tests

Soil	Sand <sup>1</sup> > 75 $\mu$ m (%)	Fines <sup>1</sup> > 2 $\mu$ m (%)	Fines <sup>1</sup> <2 $\mu$ m (%)	PI <sup>2</sup>	Soil Classification <sup>1</sup>
2	63	31	6	NP	SM-Silty Sand
3	25	49	26	17	CL-Lean Clay



# Effect of Wet or Dry Compaction is Dramatic

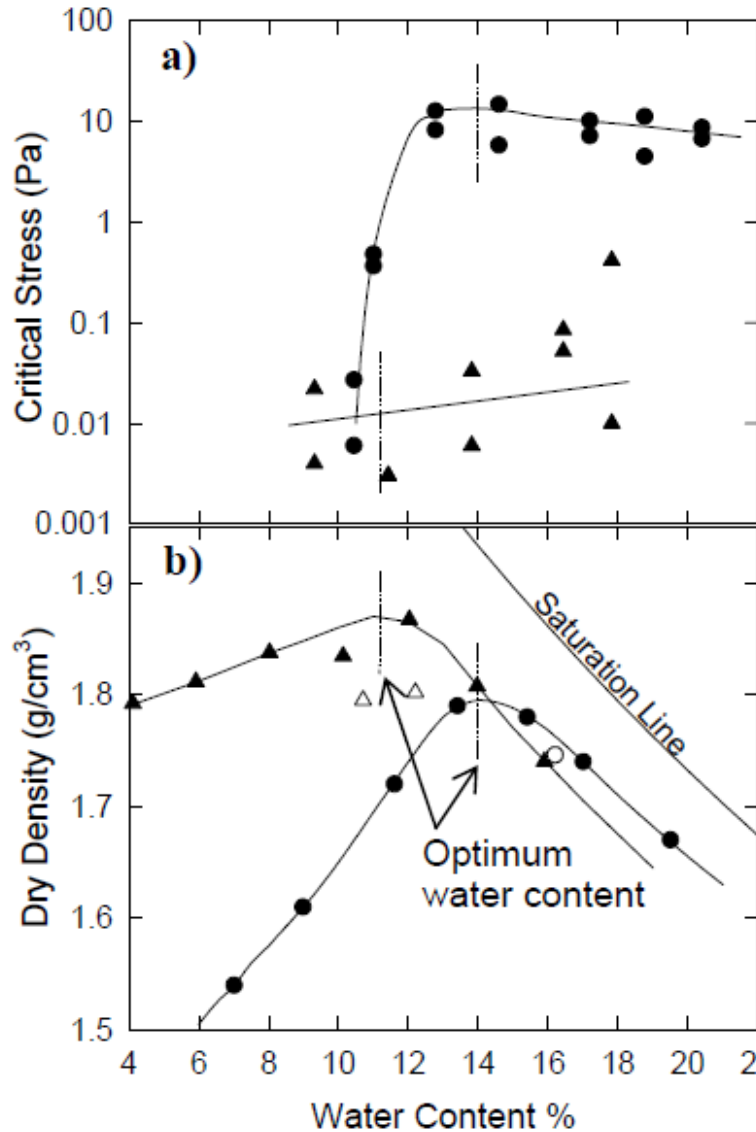


Figure 6. a) Critical stress,  $\tau_c$  vs. water content for Soil 2 and Soil 3, b) Dry density vs water content.

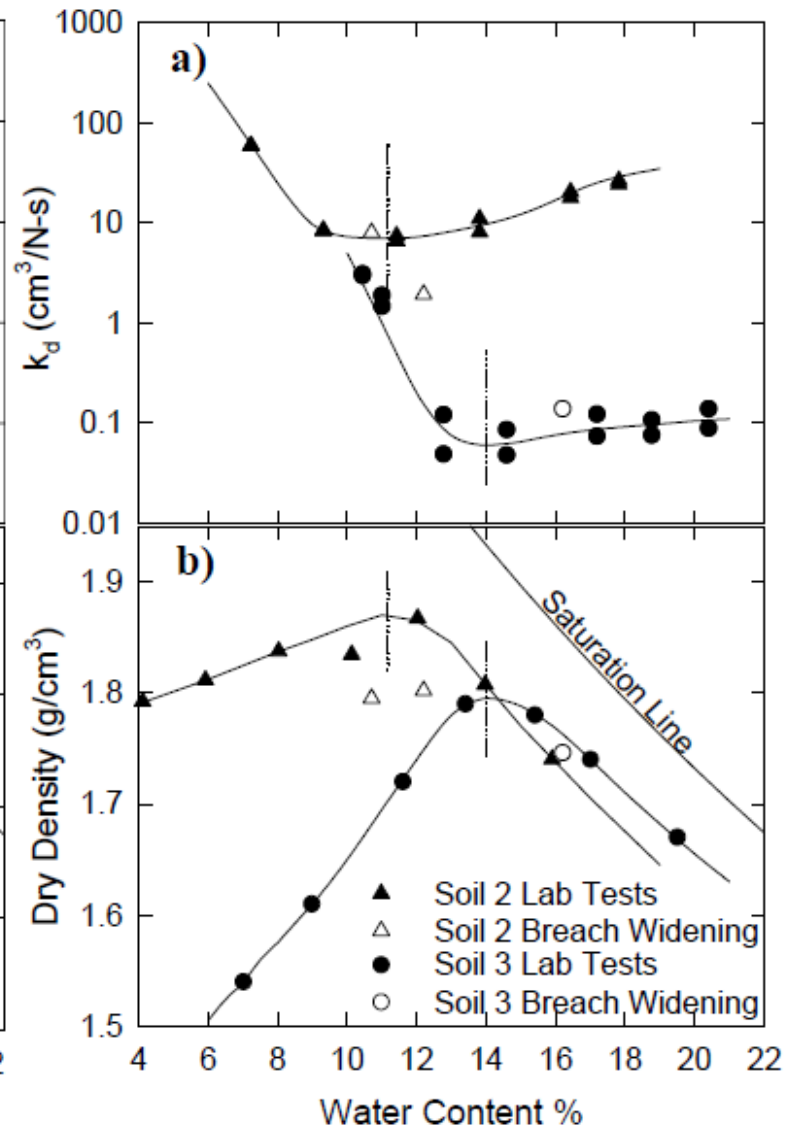


Figure 7. a)  $k_d$  vs. water content for Soil 2 and Soil 3, b) Dry density vs water content.

Compaction effort is also important

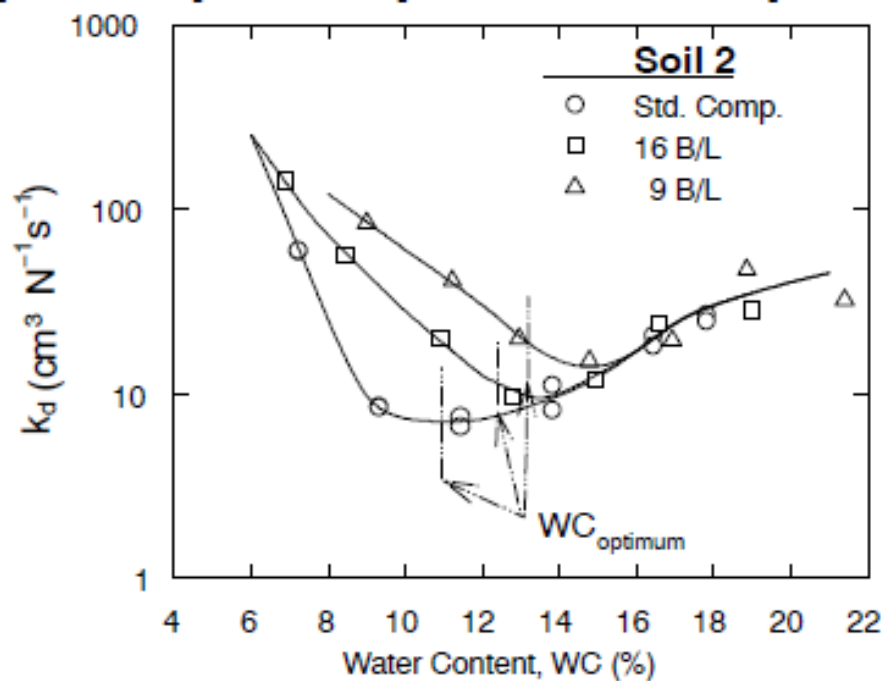


Figure 12.  $k_d$  vs. molding water content for standard, 16 B/L, and 9 B/L compaction effort of Soil 2.

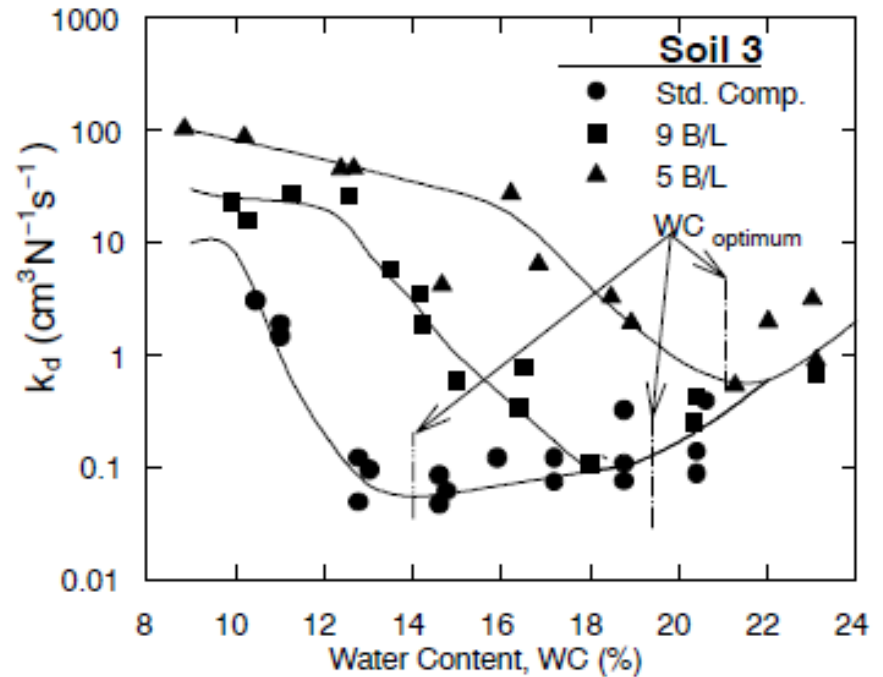


Figure 13.  $k_d$  vs. molding water content for standard, 9 B/L, and 5 B/L compaction effort of Soil 3.

Table 7. — Approximate values of  $k_d$  in  $\text{cm}^3/(\text{N}\cdot\text{s})$  as a function of compaction conditions and % clay (Hanson et al. 2010). [1  $\text{cm}^3/(\text{N}\cdot\text{s}) = 0.5655 \text{ ft/hr/psf}$ ]

% Clay ( $<0.002 \text{ mm}$ )	Modified Compaction (56,250 ft-lb/ft <sup>3</sup> )		Standard Compaction (12,375 ft-lb/ft <sup>3</sup> )		Low Compaction (2,475 ft-lb/ft <sup>3</sup> )	
	$\geq \text{Opt WC\%}$	$< \text{Opt WC\%}$	$\geq \text{Opt WC\%}$	$< \text{Opt WC\%}$	$\geq \text{Opt WC\%}$	$< \text{Opt WC\%}$
	Erodibility, $k_d$ , $\text{cm}^3/(\text{N}\cdot\text{s})$					
>25	0.05	0.5	0.1	1	0.2	2
14-25	0.5	5	1	10	2	20
8-13	5	50	10	100	20	200
0-7	50	200	100	400	200	800

Table 8. — Approximate values of  $\tau_c$  in Pa as a function of compaction conditions and % clay (Hanson et al. 2010). [1 Pa = 0.0209 psf]

% Clay ( $<0.002 \text{ mm}$ )	Modified Compaction (56,250 ft-lb/ft <sup>3</sup> )		Standard Compaction (12,375 ft-lb/ft <sup>3</sup> )		Low Compaction (2,475 ft-lb/ft <sup>3</sup> )	
	$\geq \text{Opt WC\%}$	$< \text{Opt WC\%}$	$\geq \text{Opt WC\%}$	$< \text{Opt WC\%}$	$\geq \text{Opt WC\%}$	$< \text{Opt WC\%}$
	Critical shear stress, $\tau_c$ , Pa					
>25	16	0.16	4	0	1	0
14-25	0.16	0	0	0	0	0
8-13	0	0	0	0	0	0
0-7	0	0	0	0	0	0

# Dam Breach Model Status Today

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- **WinDAM B**
  - **USDA-ARS (Stillwater, Oklahoma)**
  - **Homogeneous embankments**
  - **Vegetation or riprap slope protection**
  - **Overtopping only**
  - **Energy- and stress-based headcut erosion options**
  - **Public domain**
  - **Piping erosion module being developed...**
  - **Zoned embankments envisioned for future...**

# Dam Breach Model Status Today

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- **HR BREACH**
  - HR Wallingford
  - Homogeneous or zoned embankments
  - Vegetation or riprap slope protection
  - Overtopping and piping
  - Energy-based headcut erosion
  - Surface erosion option (for granular materials)
  - Monte Carlo simulation option
  - NOT Public domain
    - Being used in consulting
    - Being incorporated into other tools (InfoWorks RS 2D, AREBA rapid appraisal tool for homogeneous embankment breach)



# Simplified Methods

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- **When physically-based erosion and dam breach modeling is not justified or practical:**
  - Breach parameters can be predicted using established regression equations
  - Does not help address the “will it fail?” question
- **Can we put probabilities on ranges of breach parameters?**

# Probabilistic Breach Parameters

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- No work has been done that specifically assigns probabilities
- Three studies in last 10 years have addressed uncertainty of breach parameters
  - Wahl (2004)
  - Froehlich (2008)
  - Xu & Zhang (2009)

# Wahl (2004)

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- Evaluated existing breach width and breach time equations to see how accurately they predicted observed values from case studies
- Uncertainties:
  - Breach width  $\pm 1/3$  order of magnitude
  - Breach time  $\pm 1.0$  order of magnitude
  - Peak outflow  $\pm 0.5$  to  $1.0$  order of magnitude
- USBR (1988), Von Thun & Gillette (1990) and Froehlich (1995) similar for breach width
- Froehlich (1995) peak flow and time equations were superior to competitors

# Froehlich (2008)

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- **Revised breach parameter equations**
  - Breach width
  - Time of failure
  - Side slope of trapezoidal breach opening
- **Presented case study of using a Monte Carlo-type stochastic dam breach flood model**
  - Inputs were breach parameters above, plus the critical overtopping head needed to trigger failure

# Xu & Zhang (2009)

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- **Developed new equations using multi-parameter nonlinear regression techniques and different input variables**
  - dam height, reservoir shape coefficient, dam type, failure mode, and dam erodibility (high, medium, low)
  - dam erodibility was most significant factor
- **Performed uncertainty analysis to compare their equations to others**



# Breach Parameters in Risk Assessment

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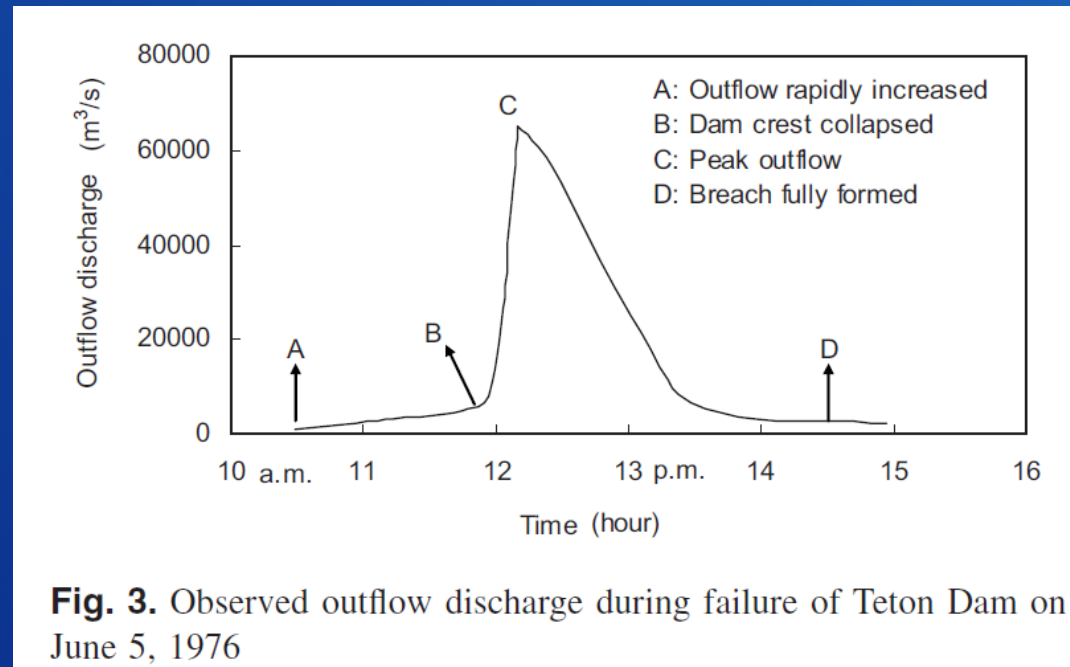
- Use uncertainty estimates and assumed probability distributions
- It is only practical to treat many parameters this way if you have a flood model that supports Monte Carlo simulation or equivalent

# Xu & Zhang (2009)

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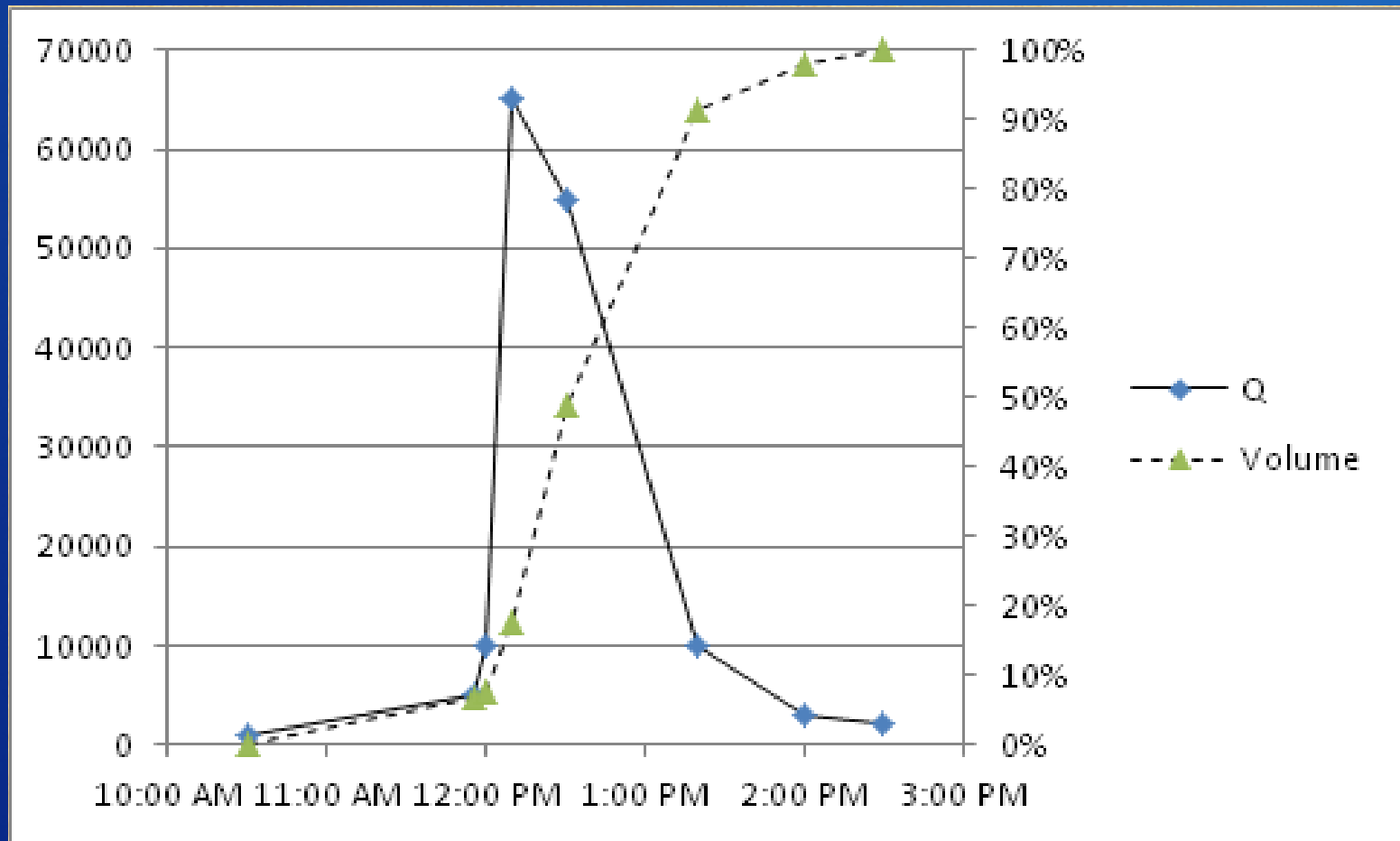
- Failure time equations should be used with caution
  - Approx. 30 dam failure cases were used to develop their failure time equations
  - 9 dams used in their analysis were also used by Froehlich (1995)
    - Same failure time for 4 of the 9
    - Dramatically longer failure times for 5 of the 9 (4x longer)
    - No specific explanation of why they differ
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# Teton Dam



- Froehlich  $T_f = 1.25$  hr
- Xu & Zhang,  $T_f = 4$  hr

# 80% of volume released in 1.5 hrs



Questions?

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